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Electric-Field Energy Harvesting From Lighting Elements for Battery-Less Internet of Things

OKTAY CETINKAYA¹, (Student Member, IEEE), and OZGUR B. AKAN², (Fellow, IEEE)

¹Next-Generation and Wireless Communications Laboratory, Department of Electrical and Electronics Engineering, Koc University, 34450 Istanbul, Turkey ²Electrical Engineering Division, Department of Engineering, University of Cambridge, Cambridge, CB2 1TN, U.K. Corresponding author: Oktay Cetinkaya (okcetinkaya13@ku.edu.tr)

ABSTRACT Internet of Things (IoT) is envisioned to bring the Internet connection to every object/ service/process to seamlessly and efficiently observe, manage, and control pervasive systems. This necessitates the employment of wireless standalone devices in excessive numbers. However, periodic maintenance of thousands, maybe millions of batteries will add massive workload and replenishment costs to the operation. In order to alleviate this problem, we introduce a totally new energy harvesting paradigm based on utilizing ambient electric-field in the vicinity of lighting elements. A low voltage prototype is designed, constituted, and evaluated on a generic $4 \times 18W$ -T8 ceiling-type fluorescent troffer. Empirical results disclose the availability of 1.5 J of energy that can be gathered in 30 min when a copper plate, i.e., the harvester, covered by a reflective dielectric is employed. The design issues to achieve the best performance attainable are addressed in both theoretical and experimental manners. The physical model of the proposed technique and an applicable circuit diagram for its execution are provided. We also point out possible application areas, and protocol stack requirements specific to our proposal to conveniently enable self-configuring IoT services, which are free from battery constraints.

INDEX TERMS Electric field, energy harvesting, wireless networks, IoT, lighting elements, fluorescent
 troffer.

16 I. INTRODUCTION

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Internet of Things (IoT) is a prominent enabling technol-17 ogy that seamlessly interconnects everyday objects to grant 18 a whole new set of benefits including numerous types of 19 services [1]-[3]. The unification of state-of-the-art technolo-20 gies has accelerated the extensive growth of IoT paradigm. 21 However, the ever-increasing number of Internet-enabled 22 devices brings along its own challenges. Even though the 23 majority of IoT devices have duty cycling, their operation 24 remarkably suffers from limited energy capabilities. This 25 issue necessitates the employment of an auxiliary and/or a 26 totally distinct power source [4]. Hence, exploiting light, 27 heat, motion, and electromagnetic (EM) radiation comes into 28 prominence to mitigate the ongoing energy constraints of 29 IoT devices. 30

The self-sufficient and maintenance-free operation of IoT paradigm can be sustained by exploiting a stray source or converting energy from one form to another. This phenomenon, i.e., energy harvesting (EH), is able to prolong the lifetime of wireless devices dramatically [5]. However, provision of perpetual and sufficient power is mostly ambiguous due to highly random and unpredictable nature of harvestable37sources. This issue brought research efforts to focus on find-38ing more reliable and efficient energy harvesting techniques.39By this means, E-field EH stands as a perfect candidate by40operating regardless of ambient parameters, providing ade-41quate power density; low complexity; and excellent energy42continuity [10].43

Preliminary studies of E-field energy harvesting are first 44 performed on power grid assets due to high-voltage resultant 45 E-field in abundance. Attractive outcomes of this method in providing advanced monitoring and intelligent control 47 accordingly directed research efforts to develop low-voltage 48 models. In this regard, lighting elements, i.e., the integral part 49 of daily human life, come to the forefront due to strong and 50 continuous E-field gradient in the vicinity [6]. This raises 51 interesting design questions to be addressed for the battery-52 less execution of IoT services. The Internet-capable and 53 E-field powered pervasive nodes actively probe the envi-54 ronment to collect information about parameters of interest, 55 process the acquired data, and notify an upper level author-56 ity for further decision making procedures. By this means,

the extension of web paradigm to monitoring, control and
management of the everyday life objects can be efficiently
maintained [2].

Even though there are several approaches to adopt E-field EH in wireless networking, there is currently no effort intended explicitly to power IoT services by utilizing illumination assets. Regarding this, and the aforementioned issues, we develop a totally new energy harvesting model that provides;

of implementation, flexibility and interrup-• ease 67 tion free operation: On the contrary of related exist-68 ing approaches, our proposal is based on embedding 69 harvesters into E-field emitting lighting elements to 70 acquire energy without effecting their operation. To do 71 that, we constituted mathematical model of the harvester 72 system and evaluated it in both theoretical and experi-73 mental manners. As a result, application specific design 74 principles are emphasized to maximize the energy to 75 be harvested, and also to allow harvesters and sensors 76 to be utilized in a more convenient and practical way, 77 i.e., deploy and forget fashion. 78

· less complex, and more efficient circuitry: As the energy 79 that can be acquired by harvesting efforts is quite limited 80 in average we tried to eliminate some energy depleting 81 but non-mandatory, i.e., optional, components to ben-82 efit more from the source being utilized. We carried 83 out several experiments with various energy storages to 84 profile the available energy. By trading on charging time 85 vs. accumulated energy the optimal storage, which satu-86 rates around the voltage that sensors operate, selected 87 to make use of any buck and/or boost type converter 88 unnecessary. The need for energy buffers, auxiliary bat-89 teries, filters and additional safety procedures are also 90 eliminated. 91

• increased luminaire efficiency: As copper plate, i.e., 92 energy harvester, to be employed has lower reflectance 93 than matt-white plane floor of fixture chest, i.e, the inte-94 gral part of energy source, we mounted the plate with a 95 non-electrical and a more reflective thin film white paper 96 to, at least, not affect the lighting process. Experimental 97 results disclosed an increment in illuminance by %5.2 98 after this alteration. 99

 highly enhanced harvesting performance: We propose an E-field energy harvesting mechanism that is able to provide roughly 1.5J of energy in every 30min.

with minimal installation, design, and maintenance costs.
The theoretical inspections and experimental findings have
predicted that the proposed method of E-field energy harvesting seems quite promising to extend the lifetime of wireless
systems. Thereby, our approach stands as a key enabler for the
pervasive deployment of self-operable and self-configuring
IoT devices.

The remainder of this paper is organized as follows. First we commence with a literature review of existing energy harvesting techniques. Then we extend our study to the theory of E-field EH, and the related existing efforts on the area. In Section III, we address fundamental design principles that 114 need to be followed, and accordingly propose a totally new 115 harvesting technique to be utilized with lighting elements. 116 This is followed by the performance analysis and a detailed 117 discussion of our proposal. While Section VI discloses the 118 possible applications that can be powered by the proposed 119 model, Section VII points out the protocol stack require-120 ments for battery-less IoT services. Finally, this paper is 121 concluded. 122

II. EXISTING ENERGY HARVESTING TECHNIQUES

Exploitable energy sources can be broadly divided into four 124 groups as light, heat, motion, and electromagnetic (EM) 125 radiation [5], in which availability, controllability, and pre-126 dictability of these sources determine the models and the 127 specifications of the harvesting procedures that are going 128 to be employed [7]–[9]. By regarding this separation, the 129 frequency of preference, and the motivation of our pro-130 posal some leading energy harvesting techniques are discussed below, and a more illustrative comparison is depicted 132 in Table 1. 133

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A. LIGHT

Power provision from light propagation means converting 135 visible lights, emitted from either sun or artificial sources, 136 into usable electric power [8]. Due to a chemical phe-137 nomenon, namely photo-voltaic (PV) effect, PV cells emit electrons when they exposed to light which yields in gen-139 erating electrical energy [9]. In outdoor, sunlight power 140 is converted by multiple PV embedded solar panels [5]. 141 However, their operation strictly depends on time varying 142 uncontrollable parameters such as weather and season. This 143 issue results in limited applicability in continuous operation 144 requiring mission critical applications [11]. In indoor, more 145 specialized photo-voltaics, which are better suited for dif-146 fused lights, are utilized for taking advantage of the rays that 147 are being emitted from artificial light sources [10]. 148

B. MOTION - VIBRATION

Kinetic energy harvesting (KEH) focuses on mechanical 150 stress and/or movement resultant motion variations and vibra-151 tions to acquire usable electrical power. The well-studied type of this method, i.e., airflow EH, is based on converting 153 wind power by using AC generators to enable wide-scale 154 communications in open areas. Besides, more specialized 155 materials, i.e., piezoelectrics, are being utilized for attain-156 ing energy from highly random and mostly unpredictable 157 kinetic sources in both indoor and outdoor domains [5], [8]. 158 Although the airflow-based systems offer sufficient power 159 conversion efficiencies, their operation is highly threatened 160 by the environmental parameters similar to sunlight-driven 161 procedures. Piezoelectric materials, in comparison, operate regardless of the ambient variables; however, fabricating 163 a generalized harvesting system, for especially vibrating 164 sources, is a challenging issue due to source specific design 165 requirements [8], [10]. 166

TABLE 1.	Comparison of	existing energy	harvesting	techniques.
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	Туре	Characteristics	Method	Power Density	Advantages	Disadvantages	Applications	Literature
Light	Solar	Solar Uncontrollable, Predictable		$\begin{array}{c} 15-100\\ mW/cm^2 \end{array}$	Environmental, Independent of grid, High output voltage	Not always available, Sensitive structure, Deployment constraints	Wireless sensors, Cellular base stations	[5], [7], [8], [9]
	Artificial	Partly-controllable, Predictable	PV Cell	$\begin{array}{c} 10-100 \\ \mu W/cm^2 \end{array}$	Abundant in indoor, Easy to implement	Low power density, Sensitive structure	Wireless sensors, Portable devices	[5], [9] [11], [12]
Temperature gradient	-	Uncontrollable, Unpredictable	Peltier, Thermocouple	$\simeq 50 \\ \mu W/cm^2$	Environmental, Low maintenance, Scalable	Not always available, Requires eff. heat sinking Low power density	On-body sensors, Wearables and consumer elec.	[5], [8], [9], [17]
Motion	Airflow	Uncontrollable, Unpredictable	Piezo Turbine, Anemometers	mW/cm^2	Environmental, Independent of grid, Available day and night	Big in size, Hard to implement, Requires construction	Wireless sensors, Cellular base stations	[7], [14] [17]
	Human-based	Controllable, Partly-predictable	Piezoelectrics	$200 \ \mu W/cm^3$	No ext. power source, Compact configuration, Light in weight	Charge leakage, Brittle materials, Highly variable output	On-body sensors, Wearable devices	[5], [8], [9], [10]
EM Waves	-	Partly-controllable, Partly-predictable	Rectenna	$\begin{array}{c} 1-10\\ \mu W/cm^2 \end{array}$	Abundant in urban lands, Allows mobility	undant in urban lands, Allows mobility Scarce in rural areas, Low power density, Distance dependent		[5], [7], [8], [12]
EM Fields	M-field	Controllable, Predictable	Current transformers	$150\ \mu W/cm^3$	No ext. power source, Easy to implement, Non-complex structure	Requires high and perpetual current flow, Safety vulnerabilities	Wireless sensors, Monitoring systems, Remote reading	[12], [14], [15], [17]
	E-field	Controllable, Predictable	Metallic plates	N.A.	No need of current flow, Easy to implement, Always available	Being capacitive, Mechanical constraints	Wireless sensors, Online surveillance	[10]–[26]

167 **C. HEAT**

Heat energy can be scavenged by benefiting from two dis-168 tinct abilities of materials, i.e., thermo-electricity and pyro-169 electricity [9]. Thermo-electricity, the most utilized, is based 170 on a physical phenomenon, namely Seeback Effect, in which 171 a junction constituted by two conductors expands in a certain 172 direction due to a thermal difference. The attained energy can 173 be easily adjusted by altering the connection of pairs as series 174 and/or parallel. Although harnessing power from temperature 175 gradients sounds promising due to its ubiquitous character-176 istic, there is a fundamental limit, namely Carnot cycle, to 177 the maximum efficiency of power extraction [8]. Due to their 178 miniature size, thermo-generators are widely used in low-179 power time-uncritical consumer electronics solutions [10]. 180

181 **D. ELECTROMAGNETIC WAVES**

With the unprecedented growth in the number of wireless 182 devices, Radio Frequency (RF) EH has received significant 183 attention in recent years [7], [8]. Due to the broadcast-184 ing nature of wireless communication, easily attainable and 185 efficiently utilizable EM waves ease the realization of 186 battery-less IoT networks. In urban areas, the ever-growing 187 RF systems are about to unseat the conventional EH methods 188 that are destined to run remote services of Smart Cities. For 189 indoor, EM signals emitted from modems, routers, smart-190 phones, and laptops are collected, and accordingly converted 191 by specialized power rectifying antennae to operate minus-192 cule of power requiring Smart Home/Building actuators. 193 RF EH provides sufficient solutions in exploiting under-194 utilized EM waves; however, its utilization is not recom-195 mended in mission-critical applications due to unpredictable, 196 distortive, and inflexible characteristics. 197

E. ELECTROMAGNETIC FIELDS

In addition to aforementioned sources, wireless autonomous devices can be also powered by profiting from electro-200 magnetic fields. Magnetic field (M-field) energy harvesting, 201 in particular, is based on coupling the outward field flow 202 of AC current carrying conductors by clamping the field 203 source with a current transformer [7], [10], [12]. This method 204 is able to provide sufficient power as long as there exist 205 adequate current flow on the conductor of interest. Being bulky and necessitating additional safety procedures, due 207 to the physical contact with high-voltage terminal, restrict 208 its employment in certain applications. However, for online 209 condition monitoring of grid assets, it outperforms many 210 techniques, i.e, sunlight and airflow EH, with its eligible 211 features. 212

E-field EH, in similar, exploits the free electric charges 213 induced on a conductive material due to a voltage gra-214 dient. On the contrary of existing scavenging procedures, 215 which require specialized harvester fabrication, E-field 216 energy harvesting is simply actualized by utilizing any con-217 ductive material available. The field that is being emitted is 218 obstructed by the conductor which results in a displacement 219 current to be drained for energy provision. E-field is the 220 only source that is neither intermittent nor dependent on 221 the load [13]. As the voltage and the frequency are firmly 222 regulated and exactingly maintained, the E-field is therefore 223 stable and predictable in its behavior [15]. It provides an 224 adequate rate of power, and has the characteristics of low complexity and excellent energy continuity. Thus, it can be 226 referred as the most promising way to compose long-term and 227 self-sustainable communication systems notwithstanding the 228 ambient factors [14]. 229

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230 III. ELECTRIC FIELD ENERGY HARVESTING - A REVIEW

According to fundamentals of electrostatics, electric charges distributed in a closed surface result in a radial E-field. This time-varying field produces an AC current I_d , i.e., displacement current, which is stated as Maxwell's following equation

$$I_d = \epsilon \int_s \frac{dE}{dt} \cdot ds$$

(1)

where ϵ is the absolute permittivity, and *E* is the electric field intensity. An apposed conductor helps I_d to drain the electric charges, and accordingly charge a storing element, C_s . The energy accumulated in this storage is expressed as

$$E = \frac{1}{2}C_s V^2$$
 (2)

where C_s is the capacitance and V is the voltage collected. As this energy is gathered by exploiting the free chargesinduced E-field, this method can be named as Electric-field Energy Harvesting (EFEH) [10]–[26].

Preliminary work on this emerging topic is first exper-246 imented on middle/high voltage (MV/HV) overhead trans-247 mission lines, utility assets and substations due to the 248 abundance of E-field formed by excessive levels of voltage. 249 As a result of high tension, sharp edges and corners needed 250 to be rounded for avoiding air ionization-based partial dis-251 charges, which yielded in tube and/or donut-shaped harvester 252 designs. The proposed harvesting model operates as a generic 253 current source to run the attached devices that monitor, pre-254 dict and identify causes of failures, i.e., sagging, icing, and 255 vibration, to maintain more reliable, high-efficient and less-256 interrupted operation. The empirical results disclosed the 257 competence of EFEH in powering the wireless devices for 258 acceptable intervals. 259

The concept of EFEH, and the corresponding tubular har-260 vester, is first disclosed by [12], in which theoretical and 261 empirical studies carried out to investigate the validity of 262 the proposed method. This discussion is further detailed 263 in [14], where a transformer-added harvesting structure is 264 experimentally evaluated. In [15], instead of utilizing a tube-265 shaped harvester, a new model based on circular metallic 266 plates is presented. Following these, the authors in [16] 267 design a multi-layer cylindrical harvester to satisfy the vary-268 ing power needs of the specialized network elements. In a 269 similar study, energy availability of the cylindrical harvester 270 is investigated with respect to capacitance variation [17]. 271 As opposed to above-mentioned approaches in the area, two 272 distinct proposals, [18], [19], represent a rectangular design 273 for ease-of-utilization, and an insulator-embedded structure 274 for enhanced security, respectively. The most recent works on 275 HV [20]–[22] are further justify the EFEH concept in building 276 wireless sensor networks (WSNs) [27] which are free from 277 battery constraints. 278

The successful trials on MV/HV eventually motivated researchers to implement the existing methods of EFEH on low-voltage (LV) systems. Although [19] declares that



FIGURE 1. (a) Conventional overhead 4-light fluorescent troffer model; (b) Harvester utilization and test circuit for the proposed E-field energy harvesting concept (patent pending design [28]).

the EFEH concept might not be a feasible option 282 for LV, this claim is invalidated by the forward research 283 efforts [23], [24], [25]. In [23], 47 μ W of power is extracted 284 with 60 cm of aluminum (Al) foil stuck on a 220V AC power 285 line. This work is taken a step further with [24], which is 286 mainly focused on enhancing the switching performance. 287 Although the harvester length is reduced to one third, from 288 60 to 20 cm, about 20 mJ of energy is scavenged in 15 min 289 with this approach. Similar method is re-handled in [25], 290 where a 60 cm long harvester, specialized for two-wire power 291 cords, is able to extract 1.4 μ W of power from a 100V AC 292 supply. Another work on low voltage is presented by [10], 293 where a multi-layer harvester destined to run more power 294 requiring network components is proposed. This approach 295 collects 12.5 mJ of energy in 15 min. As an alternative, 296 Linear Technology has brought a new perspective to the area 297 with their in-plane plates model [6]. It includes copper (Cu) 298 plate placement under fluorescent fixtures to exploit the 290 ambient field flow. This model is claimed to provide roughly 300 200μ W of utilizable power; however, the setup is bulk, hard 301 to employ, and adversely affects light propagation. A more 302 illustrative comparison of above-mentioned approaches is 303 depicted in Table 2. 304

Although there are plenty of studies on both high and low 305 voltage, none of them broadly discloses the requirements of 306 networks to be powered by this newly-emerging harvesting 307 paradigm. This work therefore addresses the challenges on network domain, investigates the applicable communication 300 architectures and outlines the possible application scenarios 310 as well as mechanical structure and circuit design consider-311 ations. The idea presented in [6], and our preliminary work 312 on this topic [26] are taken as the basis of this paper to build 313 a more flexible and efficient EFEH system for IoT-enabled 314 wireless networks. 315

IV. DESIGN OF AN E-FIELD ENERGY HARVESTER

As one of the main concerns of wireless sensor nodes is ³¹⁷ providing as much energy as possible at the smallest cost; ³¹⁸ volume; weight; and recharge time [27], an optimal harvester ³¹⁹ design is highly recommended for the best performance ³²⁰

	Literature	How the results gathered	Harvester type	Power Output	Energy Storage	Comm. Method	Voltage Output	Harvested Power/ Energy	Reporting Frequency	Application
Low Voltage	[6]	Experimentally	Two (in plane) Cu Plates	Continuous	No	N.A.	3.2V	$200 \mu W$	N.A.	Battery-less devices
	[10]	Experimentally	Double-layered Cylindrical Al/Cu Sheets	Intermittent	Capacitor $(2.2 \mu F)$	Internet -based	3V	12mJ	15min.	WSNs for Smart Grid (SG)
	[23]	Experimentally	Cylindrical Al Foil	Intermittent	Capacitor $(47 \mu F)$	RF -based	10.9V	$47 \mu W$	42sec.	WSNs for SG
	[24]	Experimentally	Cylindrical Cu Sheet	Intermittent	Capacitor $(100\mu F)$	ZigBee	3.3V	20mJ	300sec.	Home automation, Smart Grid
	[25]	Experimentally	Semi tubular Two Cu Sheets	Intermittent	Capacitor $(100 \mu F)$	ZigBee	4V	$1.4 \mu W$	250sec.	Building energy management
	[26]	Theo./Exp./Sim.	Cu Plate	Intermittent	Super-capacitor (0.1F)	Internet -based	5V	1.25J	N.A.	IoT networks
Middle Voltage	[18]	Theo./Sim.	Cylindrical Al Electrode	Continuous	No	N.A.	N.A.	100mW	N.A.	Smart Grid monitoring networks
	[19]	Theo./Exp./Sim.	Al box	Continuous	Capacitor $(330\mu F)$	ZigBee	3V	17mW	N.A.	SG sensors for MV/HV assets
	[20]	Theoretically	Cylindrical Al Electrode	Continuous	No	N.A.	13V	17mW	N.A.	Power-line monitoring for SG
	[22]	Theo./Exp./Sim.	Two Cylindrical Electrodes	Intermittent	Super-capacitor (0.47F)	RF -based	3.26V	110mW	90min.	Battery-less monitoring of SG assets
High Voltage	[12]	Theo./Sim.	Two Plates (Parallel)	Continuous	No	N.A.	N.A.	95mW	N.A.	WSNs in power systems
	[14]	Exp./Sim.	Cylindrical Electrode	Continuous	No	RF -based	9V	370mW	N.A.	Online condition monitoring of HV power lines
	[15]	Theo./Exp./Sim.	Two Circular Plates (Parallel)	Intermittent	No	N.A.	N.A.	10.6mJ	1 min.	Wireless condition monitoring sensors
	[16]	Theoretically	Cylindrical Electrode	Intermittent	Capacitor $(0.1 \mu F)$	N.A.	N.A.	N.A.	N.A.	Power-line monitoring networks
	[17]	Theo./Exp./Sim.	Cylindrical Electrode	Intermittent	Super-capacitors (3.6F)	N.A.	5.5V	$16.4 \mathrm{mW}$	20min.	Power-line monitoring networks
	[21]	Experimentally	Plate	Continuous	No	N.A.	N.A.	645 mW	N.A.	Online condition monitoring

TABLE 2. Comparison of existing E-field energy harvesting approaches.

attainable. Now, consider a system of one conductive plate, 321 specifically copper, closely placed under an overhead flu-322 orescent troffer in parallel, as roughly depicted in Fig. 1. 323 The copper plate placed obstructs the time varying flow of 324 E-field around the fluorescent tubes, where the field induced 325 electric charges are transferred by a displacement current 326 I_d . As this plate capacitively divides the ground-to-fixture 327 potential, I_d accordingly charges the capacitors formed by 328 the copper plate. In other words, splitting up the field by 329 conductors not only results in a voltage difference, but also 330 forms parasitic in-plane capacitances which are energized 331 by capacitive coupling. A more illustrative representation of 332 the above-mentioned scenario and distribution of the formed 333 stray capacitances are depicted in Fig. 2(a), (b). 334

With respect to our measurements and the fundamentals 335 of electrostatics, fluorescent tubes are assumed as uniform 336 sources of E-field to simplify the model given by Fig. 2(b), 337 and therefore reduce the computational complexity of theo-338 retical consideration. As seen in Fig. 2(c), the plate placed 339 between the ceiling and fluorescent tubes acts as a voltage 340 divider, and in this circumstance the major contributions are 341 only due to one C_f and a serially connected C_h . It should be 342 noted that the fringing capacities, and also the other fringing 343 resultant factors are neglected in the following theoretical 344 investigation. 345

The equivalent impedance of the simplified model Z in Fig. 2(c), and the voltage u on the load Z_L are obtained VOLUME 5, 2017 as

$$Z = \frac{Z_L}{1 + jwC_h Z_L} + \frac{1}{jwC_f} \quad [\Omega]$$
(3) 345

$$u = u_0 \left(\frac{j w C_f Z_L}{1 + j w Z_L (C_f + C_h)} \right) \quad [V] \tag{4}$$

where u_0 and w represent phase-to-ground rms voltage and assumption angular frequency of the power-line, respectively.

The capacitance from bulb to harvester, i.e., C_f , can be stated as 353

$$C_f = \frac{2\pi\epsilon l}{\cosh^{-1}(d/r)} \quad [F] \tag{5} \quad 355$$

where l is the tube length, r is the tube radius, and d ³⁵⁶ refers to vertical distance from tube to plate. Similarly, the ³⁵⁷ capacitance from harvester to ground, i.e., C_h , can be given ³⁵⁸ as ³⁵⁹

$$C_h = \frac{2\pi\epsilon l}{\ln(2H/r)} \quad [F] \tag{6} \quad {}_{360}$$

where *H* denotes the distance from tube's center to ground. Note that, ϵ means absolute permittivity, i.e, $\epsilon = \epsilon_0 \epsilon_r$, where ϵ_0 and ϵ_r refer to vacuum and relative permittivities, respectively. As tube-to-ground distance is quite small in our approach, the resting capacity is calculated by considering the voltage difference between the harvester and ground planes.

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FIGURE 2. (a) Cross section depiction of 4-light fluorescent troffer with harvesting plate placement; (b) Physical model of the proposed EFEH concept; (c) Simplified model of the proposed EFEH concept.

The voltage u on the load Z_L are re-expressed in (14), 368 as shown at the bottom of this page, by inserting (5) and (6) 369 into (4). By substituting constant values in (14) with 370

$$\int m = \ln(2H/r)2\pi\epsilon l \tag{7}$$

$$\begin{cases} k = \ln(2H/r)\cosh^{-1}(d/r) & (8) \\ a = 2\pi\epsilon l(H-d)\cosh^{-1}(d/r) & (9) \end{cases}$$

$$a = 2\pi\epsilon l(H-d)\cosh^{-1}(d/r)$$
(9)

the load voltage *u* can be therefore simplified as

$$u = u_0 \left(\frac{jwZ_Lm}{k + jwZ_L(a+m)}\right) \quad [V]$$
(10)

If Z_L is assumed as an ohmic load, the obtainable power 374 from the harvester can be calculated as 375

³⁷⁶
$$P = \frac{|u|^2}{Z_L}$$
 [W] (11)

When $\partial P/\partial Z_L = 0$, the optimal load impedance $Z_{L_{opt}}$ can 377 be found by 378

$$Z_{L_{opt}} = \frac{k}{w \cdot (a+m)} \quad [\Omega] \tag{12}$$

where the maximum achievable power is therefore calculated 380 by substituting Z_L by (12) in (11), i.e., $P_{max} = P(Z_{L_{opt}})$, as 381

₃₈₂
$$P_{max} = P(Z_{L_{opt}}) = \frac{Z_{L_{opt}}(wmu_0)^2}{k^2 + (w(a+m)Z_{L_{opt}})^2}$$
 [W] (13)

From (13), also considering (7), (8) and (9), it can be said 383 that the maximum achievable power P_{max} increases with the 384 rms voltage of the power-line u_0 , relative permittivity ϵ_r ; and 385 decreases with the distance from tubes to plate d; however, 386 it has a convex behavior for load resistance R. Fig. 3 rep-387 resents the variation in obtainable power P with respect to 388 voltage u_0 , load resistance R, relative permittivity ϵ_r , and 389 distance d, respectively. 390

In addition to above-mentioned metrics, to extract more 391 power from the surrounding field, the harvester must be 392 perpendicular to the tubes, and the size of it must be as large 393

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as possible. To validate these, we performed complementary 394 experiments. As seen in Fig. 4, the proposed model is tested 395 for three different scenarios, i.e., varying angular aperture, 396 plate area, and E-field intensity. In the first case, Fig. 4(b), the angular aperture between the harvester and fluorescent 398 bulbs is increased from 0° to 30° and 60° , respectively. In the second case, Fig. 4(c), the plate area is altered by an 400 increment of $\simeq 200 \text{cm}^2$. In the last scenario, Fig. 4(d), the 401 number of light emitting fluorescent bulbs are changed to 402 observe the alteration in obtainable power with respect to 403 E-field intensity.

By regarding theoretical investigation, dimensional limits 405 of the fluorescent fixture, and the corresponding results given 406 in Fig. 4(e),(f),(g), the size, position and the structure of 407 the E-field energy harvester can be determined to obtain 408 the best performance achievable. These aspects can be also 409 regarded as fundamental guidelines for the design of battery-410 less sensory structures and/or wireless services. In this sense, 411 any AC-powered lighting element can be conveniently turned 412 into a generic power source without any effect in its operation. 413 This issue is expected to revolutionize the structure of today's 414 battery-constrained communication architectures. 415

V. PERFORMANCE EVALUATION

In order to test the validity of our proposed model, a conven-417 tional 4 \times 18W-T8 type 60 \times 60 \times 10cm overhead fluorescent 418 troffer is utilized. To prevent a galvanic contact with the 419 fixture, providing ease of implementation, and to enable the 420 best performance achievable the copper plate is adjusted as 421 50×50 cm in size, and placed 1cm away from the fluorescent 422 bulbs as in Fig. 2(a) by regarding the design aspects disclosed 423 in Section IV. The diagram seen in Fig. 1(b) refers to a test 424 circuit utilized for the preliminary experiments, which is fur-425 ther improved as in Fig. 5(c) to constitute a more generalized 426 harvesting system. 427

The main objective of the conceptual model given in 428 Fig. 5(c) is to drain I_d and collect the charges in C_s , until 429

$$u = u_0 \cdot \frac{jw 2\pi \epsilon l \ln(2H/r) Z_L}{\ln(2H/r) \cosh^{-1}(d/r) + jw Z_L [2\pi \epsilon l \ln(2H/r) + 2\pi \epsilon l \cosh^{-1}(d/r)]}$$
[V]

(14)



FIGURE 3. (a) Maximum available power P_{max} [W] vs. nominal voltage u_0 [V]; (b) obtainable power P [W] vs. load resistance R [M Ω]; (c) obtainable power P [W] vs. relative permittivity ϵ_r ; (d) obtainable power P [W] vs. distance from tubes to harvester d [m].



FIGURE 4. (a) Representative depiction of the E-field lines on a cylindrical source, i.e., fluorescent tube; (b) Testbed for angular aperture; (c) Testbed for plate area; (d) Testbed for field intensity, i.e., voltage source; (e) time vs. accumulated voltage for varying angles; (f) time vs. accumulated voltage for varying plate sizes; (g) time vs. accumulated voltage for varying number of fluorescent tubes.

the stored energy becomes sufficient for sensing; processing; and transmission. The copper plate obstructs the time-varying flow of E-field in the vicinity of the fluorescent fixture, which is followed by concentrating the acquired electric charges into C_{in} after being rectified. The rectifier is for both converting the alternating current, and preventing the scavenged energy from back feeding [4].

The block stated as ACC in Fig. 5(c), i.e., autonomous con-437 nection circuit, is for switching between harvesting and nodal 438 operation stages [19], [29], [30]. This circuit simultaneously 439 compares the voltage on input storage C_{in} and accordingly 440 enables charge transfer to the primary storage C_s when the 441 harvested energy is sufficient enough for nodal operation. 442 Then it disengages C_s from the circuitry for turning back 443 to harvesting period when the voltage drops below a certain 444 threshold. This operation not only prevents the undesired 445 discharge of C_s , but also allows more frequent transmissions 446 as the time spent on harvesting stage is shortened. It should 447 be noted that this process can be either performed by a 448 low-power processor, a distinct one or the attached device's, 449

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or by a simple circuitry which offers a more robust solution. ⁴⁵⁰ The given regulator block adjusts the output voltage of the ⁴⁵¹ harvester system for the wireless device to be attached. Both ⁴⁵² C_{in} and C_s can be selected as same-featured super-capacitors ⁴⁵³ without loss of generality. ⁴⁵⁴

As the energy that can be gathered by harvesting tech-455 niques is mostly limited, utilization of low-loss rectifiers; 456 power-saving processors; and more efficient regulators are 457 highly recommended. In other words, from beginning to 458 end each process requires the most efficient operation 459 possible [4]. Since, any decrease in the amount of energy 460 consumed on the harvester side directly affects the sensor 461 lifetime, which will accordingly increase the communication 462 reliability. It is also essential to enhance the energy storage 463 capabilities to alleviate the rising demand for better lifespan. 464 Thus, super-capacitor employment is highly recommended due to their more charge/discharge cycles; higher efficiency; 466 and longer lifetime characteristics. In addition to each com-467 ponent being optimized for low power consumption, intelli-468 gent system/stage-level power-saving algorithms should be 460



FIGURE 5. (a) Measurement setup -with paper mounting; (b) time vs. accumulated voltage & energy on C_s; (c) Equivalent circuit diagram of the proposed EFEH concept.

470 also developed and integrated into both hardware and soft471 ware design of EFEH-powered IoT devices for enhanced
472 longevity [31].

In order to estimate the energy profile of our harvester sys-473 tem, and accordingly determine the circuitry to be employed 474 a series of experiments were performed. We tested a plethora 475 of capacitors and analyzed their performance in terms of 476 charging time versus accumulated energy. The preliminary 477 results revealed that, it is possible to gather 1.5J of energy, 478 on average, in 30min with our proposed harvesting model, 479 i.e., 0.5J of energy in 15min, Fig. 5(b). In the light of this 480 outcome, 0.11F of super-capacitor is selected for the storage 481 as it saturates roughly at 5V which is the exact voltage 482 required by a great majority of sensor nodes on the com-483 mercial domain [10]. Therefore, employing any converter-484 like component to further adjust the output voltage becomes 485 unnecessary. As the ongoing circuit complexity constraints 486 of conventional harvesters can be resolved, the rate of power 487 transferred to the load can be also enhanced by this approach. 488 As a result, 3.3V level is set as sub-limit for nodal operation, 489 which determines duty cycle of the proposed EFEH system. 490 The result, Fig. 5(b), points out to a remarkable improvement 491 for the concept of energy harvesting when the existing power 492 provision architectures are considered. 493

The proposed harvesting procedure enables ease of 494 employment due to the neutral bus situated in the vicin-495 ity of the fluorescent fixture. In other words, there is no 496 need for peeling of concrete surface and/or dealing with 497 cabling to complete the harvesting circuitry on the contrary 498 of existing efforts [23], [24]. This design also offers a more 499 secure implementation due to necessitating no galvanic con-500 tact with the field emitting parts unlike magnetic field-based 501 counterparts [12]. 502

To ensure interruption-free operation, we further improved 503 our model and performed additional experiments for its val-504 idation. As copper plate has a much lower reflectivity in 505 contrast with the matt-white plane floor of the fixture chest, 506 it is expected that copper placement may adversely affect the 507 luminaire efficiency. To at least not decreasing it, we mount 508 the plate with a non-electrical and a more reflective white 509 paper as seen in Fig. 5(a). The measurements taken by a lux 510

meter point out to an increase in illimunance by 5.2%, i.e., 511 from 984 to 10351x at a vertical distance of 60cm. As the 512 theoretical consideration discloses, negligible increment in 513 the absolute permittivity due to dielectric placement results 514 in a negligible increment in the amount of harvested energy, 515 but a considerable change in luminaire efficiency. Contrary 516 to expectations, the empirical results show that this newly-517 constituted configuration not only operates without affecting 518 the illumination process but also offers increased luminaire 519 efficiency in contrast with [6]. 520

The proposed model also stands as an interdisciplinary 521 effort which opens up the potential of a hybrid harvest-522 ing technology for IoT devices/services [11]. As a certain 523 portion of energy is dissipated as heat during illumination, 524 harvester can be structured as enabling power extraction 525 from temperature gradients as well as electric fields. Further-526 more, the lights emitted from fluorescent tubes can be also 527 exploited if the harvester is structured with the capability of 528 PV conversion. 529

By taking this potential into account it can be said that 530 this approach can contribute to maximize the efficiency of 531 power extraction process, as well as decreasing the level 532 of energy wasted during illumination. We hereby obtain 533 a unique solution that offers flexible, safe, cost efficient 534 and interruption-free operation while providing a remarkable 535 amount of energy, which therefore stands as a shoo-in for 536 broadening the scope of energy harvesting communications. 537

VI. POSSIBLE APPLICATION AREAS OF IOT-ENABLED EFEH WIRELESS NETWORKS

For home and building area network (HAN/BAN) scenar-540 ios [32], [33], the foreseen charging time, i.e., reporting 541 frequency, of our proposal seems quite acceptable as the exe-542 cuted tasks are neither mission/time critical nor high energy 543 consuming in general, Table 3, [10]. The EFEH-powered 544 networks structured with specialized sensors may help to 545 prevent the wastages; minimize the losses, and increase the 546 operational efficiencies by managing the operation of such 547 systems like air-conditioning, heating and lighting in resi-548 dential and commercial buildings. A detailed consumption profile can be constituted for both demand responsive 550

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	Network Type	Service	Typical Packet Size (bytes)	Reporting Frequency	Tolerable Delay	Communication Technologies	Energy Source	
Smart Home/Building	HAN BAN	Home Automation	10-100	15 min.	2 min.	Z-Wave, Bluetooth, ZigBee, Wi-Fi, 3G, 4G	Battery powered or energy harvester	
		Building Automation	> 100	15 min.	2 min.	ZigBee, Wi-Fi, Wireless Mesh, 3G, 4G	Mains powered or energy harvester	
Smart City	NAN FAN	Structural Health	100	10 min.	30 min.	802.15.4, Wi-Fi, Ethernet	Battery powered	
		Air Quality Control	25 - 255	30 min.	5 min.	802.15.4, Bluetooth, Wi-Fi	Battery powered or energy harvester	
		Noise Monitoring	255	10 min.	5 min.	802.15.4, Ethernet	Battery powered or energy harvester	
		Traffic Congestion	255	10 min.	5 min.	802.15.4, Bluetooth Wi-Fi, Ethernet	Battery powered or energy harvester	
		Smart Lighting	100	On demand	1 min.	802.15.4, Wi-Fi, Ethernet	Mains powered or energy harvester	
		Smart Parking	150 - 250	On demand	1 min.	802.15.4, Ethernet	Energy harvester	
Smart Grid	WAN	Demand Response	100	60 min.	> 5 min.	ZigBee Mesh, WiMax, Wi-Fi Mesh, Cellular	Energy harvester	
		Situational Awareness	4 - 157	> 2 min.	1 min.	WiMax, Cellular	Energy harvester	
		Wide Area Monitoring	> 52	> 2 min.	> 0.5 min.	WiMax, Cellular, Satellite communication	Energy harvester	

TABLE 3. Network requirements/specifications of some commercial wireless services [3], [32]–[34].

reactions and future saving behaviors. As Table 3 suggests, 551 the very same approach sounds also promising for the 552 energization of widespread elements deployed in out-553 door. This result accordingly encourages the establish-554 ment of low-power field, near and wide area networks 555 (FANs/NANs/WANs), which reveals the possible coverage 556 of all networking schemes taking part in the Smart Grid 557 architecture [33]. 558

Although Smart Grid vision proposes a reliable connection 559 between a large number of diverse elements that are geo-560 graphically spread [2], this connection is still a challenging 561 issue due to the limited capabilities of existing communi-562 cation protocols. At that point, insertion of newly-emerging 563 IoT paradigm into the SG domain poses a huge potential to 564 bring a rich set of advantages such as enhanced management 565 and seamless interoperability, besides broad connectivity. 566 With IoT, it becomes possible to connect evenly-distributed 567 plethora of elements in a convenient and efficient way. The 568 crucial data related to any system part can be transferred, 569 when and/or where it is necessary, over the shortest link pos-570 sible with a minimum expense of power and delay. The con-571 siderably enhanced communication parameters, and better 572 coordinated and interconnected network structure facilitate 573 the intelligent monitoring, control and maintenance of grid 574 assets with the adaption of self-configuring versatile devices 575 that EFEH offers. 576

Although the employed testbed sounds like targeting 577 indoor applications, it can be easily adapted into outdoor 578 systems since lighting is an essential part of daily human 579 life. In this context, the major Smart City services, i.e., 580 smart lighting; smart parking; traffic congestion tracking; 581 noise, air quality and structural health monitoring [34], can 582 be performed by EFEH-powered IoT. For example, EFEH-583 capable vibration, deformation, humidity and temperature 584 sensors can sense the parameters of interest, and real-timely 585 notify city authorities about the stress and the environmental 586

conditions that the structures are exposed. This better forecast will eventually contribute to reduce periodic maintenance and control costs. 587

Instead of using bulky and sunlight-depended solar panels, EFEH-powered sensor nodes situated on field emitting street-591 lights can reliably measure air quality in public places. The 592 measurements can be uploaded to a cloud-based database 593 for public awareness. Battery-operated noise sensors can be 594 also substituted by EFEH devices to reduce noise levels in cities at specific hours [34]. Similarly, highway lightings can 596 be utilized to employ EFEH procedures that energize traffic congestion control mechanisms. Furthermore, the proposed 598 method of EFEH can be also beneficial for smart lighting 599 applications in cities. Regarding to measurements taken by 600 light, weather, and proximity sensors, light intensities can 601 be optimized for increased energy consumption efficiency. 602 All these alterations are intended to make a better utilization 603 of city resources and increasing the quality of city services, 604 while minimizing costs and causalities, and maximizing oper-605 ational efficiencies [34]. As it is revealed by the experiments, 606 the proposed method of EFEH is able to run a majority of 607 Smart Home/Building, Smart City and Smart Grid services. 608 It refers that any E-field emitting light source will therefore become an integral part of these pervasive heterogeneous 610 networks by allowing sensors to be attached conveniently. 611 By taking into account all of these results, it can be said 612 that this promising candidate will considerably change the 613 operation of existing IoT-enabled Smart Home/Building, City and Grid networks in the very near future. 615

VII. PROTOCOL STACK REQUIREMENTS OF THE IoT-ENABLED EFEH COMMUNICATIONS

Due to the inherent limitations of EH paradigms, conventional communication architectures need to be exactingly modified as being extremely efficient. Although the EFEH methods are developed to alleviate insufficient storage

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capabilities of generic batteries and/or limiting intermittency 622 of current EH techniques, they have not been entirely utilized 623 in the IoT domain. As our intention is battery-less execution 624 of IoT services, existing communication technologies should 625 be revisited to enable self-operable and self-configuring 626 IoT networks, which requires the highly optimized versions 627 of Internet protocols [2]. Hence, this issue necessitates recon-628 struction of all network layers, i.e., protocol stack of the IoT, 629 in an energy-aware and power-efficient fashion. 630

631 A. PHYSICAL LAYER

Utilization of lighting elements for power extraction neces-632 sitates the physical layer of existing IoT networks to be 633 rehandled as a new design problem. As this newly-emerging 634 method is totally different from traditional battery and/or 635 energy harvesting powered communications, new mod-636 els and optimal transmission policies are highly required 637 to maximize the throughput, reliability and quality of 638 service (OoS). 639

The proposed model of EFEH is tailored to overcome the 640 restrictions posed by the limited energy storage capabilities 641 of wireless devices in IoT applications. Due to its diverging 642 nature, the existing well-applied communication architec-643 tures must be restructured to make self-operable IoT networks 644 implementable in practice. In addition, the amount of data 645 that can be transmitted with the minimum energy harvested 646 should be maximized to further increase the lifetime of sensor 647 nodes. 648

To determine the capacity, communication channel should 649 be modeled and accordingly analyzed by regarding the 650 amount of energy scavenged. In addition to energy-aware 651 coding schemes, more simpler and harvesting adaptive mod-652 ulation techniques should be also investigated to provide 653 an energy-efficient communication architecture. Less com-654 plex; more compact; and less power consumptive ultra-low 655 power (ULP) transceivers need to be developed to boost the 656 longevity. 657

658 **B. DATA LINK LAYER**

The continuous and reliable profile of the energy captured by 659 exploiting lighting elements paves the way for perpetual data 660 transmission, i.e., real-time monitoring, control and manage-661 ment activities. As the proposed method is able to offer much 662 more energy than the existing power provision schemes by 663 nearly acting like a continuous current source, it becomes 664 possible to increase the transmit power (P_t) without any effect 665 on sensor's lifetime. An increased P_t means more power to be 666 received P_r , and an increased signal-to-noise (SNR) ratio on 667 the receiver side. More SNR point out an increment in the 668 channel capacity, i.e., an enhanced throughput. In addition, 669 it can also be featured for decreasing the number of faulty 670 transmissions, which reveals a need for the reassessment 671 of current error control mechanisms. As a myriad of error 672 correcting methods may become implementable depending 673 on the accumulated energy, a detailed inspection of possible 674 trade-offs between power consumption and reliability need to 675 be maintained. 676

Since the ever-growing number of wireless devices is expected to reach to a new level with the emergence of IoT concept, unacceptable queues and delays in data transmission will be inevitable. This issue will incapacitate the spectrum, which is densely populated even now, in the very near future. To resolve this problem, previously proposed spectrum-aware solutions [35], [36] must be revisited in an energy-efficient manner.

Although the duty cycle for data transmission should be kept as low as possible due to relatively high power consumption in wake-up, listen and receive/transmit stages, the node must be responsive enough to help better anticipate a likelihood of a sudden request to ensure lossless reception/ transmission of a packet. This issue necessitates tightengineering for power-saving data link layer technologies to efficiently interconnect different IoT components.

In addition to aforementioned aspects, medium access control (MAC) stands as an another challenging issue in the realization of Internet-enabled self-sustaining wireless autonomous devices. More optimal and energy-efficient MAC protocols must be developed by regarding the capabilities of this newly-emerging energy harvesting procedure.

C. NETWORK LAYER

As addressed in Section V, a prototype is designed, fabricated 700 and tested on a conventional ceiling type fluorescent 701 troffer to validate the feasibility of the proposed idea. 702 However, the nature and the corresponding illumination requirements of the residential and commercial buildings, 704 public places, parks, and/or stadiums are envisioned, it can be mentioned about numerous types of utilizable light fixtures, 706 i.e, a plethora of ambient E-field sources. Employment of 707 these assets for power provision will result in a variance 708 in the amount of harvested energy due to the variety of 700 exploited sources' characteristics. This issue causes a very dynamic environment for routing solutions in IoT-enabled 711 EFEH networks. Thus, network layer should be structured 712 by considering the competence of this proposed scavenging 713 mechanism. Energy-aware routing and delay-tolerant for-714 warding algorithms need to be procured. 715

More specifically, for data centric and flat architecture 716 protocols, the nodes with more energy harvested should 717 participate in the routing process. With a precise knowl-718 edge of instant energy-levels, the protocols will be able 719 to route the data through large multi-hop topologies with-720 out any packet drops. For hierarchical routing algorithms, 721 cluster-heads should be selected among the nodes that have 722 the highest energy levels in their neighborhood, due to 723 the high power demanding two-sided communications that 724 cluster-heads are obliged to perform. This issue necessi-725 tates the consideration of energy-aware clustering mecha-726 nisms. Location-based routing algorithms in particular seems 727 promising for EH-powered IoT applications as being energy 728 efficient; however, delivering periodic location information 729 might be difficult for densely-populated networks. In addi-730 tion, QoS-driven routing algorithms might be also beneficial 731

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to meet the network layer requirements of major IoT services 732 by keeping in mind the capabilities of our proposal. 733

D. TRANSPORT LAYER 734

As the network to be structured is foreseen as a compose of 735 heterogeneously powered devices, it is probable for a node 736 to have inadequate energy when it is supposed to relay an 737 upcoming datum to the next recipient. This mismatch might 738 also occur due to the executed operation stage, deep sleep or 739 lack of proper acknowledgment. Therefore, synchronization 740 points out a crucial issue related to transport layer what needs 741 to be developed as adaptive to the energy levels of network 742 components. In addition, less power consuming transport 743 control protocols (TCP) and energy-aware congestion detec-744 tion algorithms needs to be studied. 745

The reliable delivery of data packets to gateways in IoT 746 domain depends on a variety of parameters, in which the 747 energy levels of relay nodes come to the forefront due to 748 the diverse specs of lighting elements to be utilized. For the 749 best performance achievable, efficient interaction between 750 energy-aware network layers, hence cross-layer communi-751 cation solutions must be investigated. They should con-752 sider the heterogeneity in the capabilities of IoT devices 753 to propose novel algorithms that decreases energy con-754 sumption, provide seamless Internet connectivity and satisfy 755 desired QoS requirements. Furthermore, both EH techniques 756 and harvesting-adaptive communication protocols need to 757 be standardized to assure the compatibility of EH devices 758 in commercial domain, conveniently manage the network, 759 reduce the overall heterogeneity, and mitigate the inefficien-760 761 cies occurred by existing cross layer protocols.

VIII. CONCLUSION 762

This paper proposes a novel power provision architecture that 763 is based on exploiting E-fields emitted by lighting elements. 764 Fundamental requirements of IoT-enabled self-sustainable 765 devices are addressed in both hardware and networking terms. 766 Design aspects that maximize the harvesting efficiency are 767 theoretically and experimentally evaluated. A low voltage 768 prototype is outlined, structured and tested on a conventional 769 overhead fluorescent fixture. Empirical findings disclose the 770 potential of this proposed scavenging alternative for the 771 applications in which greater longevity; higher robustness; 772 and larger throughput are essential. It is believed that this 773 effort will mitigate the energy constraints of wireless net-774 works in the very near future by substituting the batteries 775 without any effect on system performance. It is also envi-776 sioned that this approach will broaden the scope of energy 777 harvesting procedures, and ease the building of self-operable 778 IoT services. 779

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OKTAY CETINKAYA (S'13) received the B.Sc. 890 degrees in electrical engineering, and electron-891 ics and communication engineering from Yildiz 892 Technical University, Istanbul, Turkey, in 2013 893 and 2014, respectively. He is currently pursuing 894 the Ph.D. degree with the Electrical and Elec-895 tronics Engineering Department, Koc University. 896 He is currently a Research Assistant with the Next-generation and Wireless Communications 898 Laboratory, Koc University. His current research 899

interests include energy harvesting communications in smart environments with advanced energy management, monitoring, and control systems. 901



OZGUR B. AKAN (M'00-SM'07-F'16) received 902 the Ph.D. degree in electrical and computer 903 engineering from the Broadband and Wireless 00/1 Networking Laboratory, School of Electrical and 905 Computer Engineering, Georgia Institute of Tech-906 nology, Atlanta, GA, USA, in 2004. He is 907 currently with the Electrical Engineering Divi-908 sion, Department of Engineering, University of 909 Cambridge, U.K. His research interests include 910 wireless, nano, molecular communications, and 911 Internet of Everything. 912